

Jagiellonian Symposium on Fundamental and Applied **Subatomic Physics**

Development of a dedicated beam forming system for material and bioscience research with high intensity, small field electron beam of LILLYPUT 3 accelerator at Wroclaw Technology Park

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The LILLYPUT 3 electron accelerator designed and manufactured at National Centre for Nuclear Research in Swierk, Poland (NCBJ) is the principal instrument of The Nondestructive Testing Laboratory at Wroclaw Technology Park.

The accelerator delivers 6 and 9 MeV electron beams. In a standard configuration the electron beam is converted into X-ray beam in a water cooled tungsten target. The primary use of the accelerator is nondestructive testing including R&D of novel techniques for industrial and medical imaging.

In addition, the high intensity electron beam can be directly extracted for a broad range of applications including material and bioscience research. For those applications a specialized beam forming system has been designed at NCBJ.

The purpose of this system is to deliver as high intensity electron beam as possible, while keeping beam flatness within 10% on a 7x7 sq. cm field in the distance of 40 cm from the beam exit window. Two alternative solutions were taken into consideration, one involving beam scanning and second based on passive beam forming with flattening foil. While it seemed that the highest beam intensity can be achieved by beam scanning, the in-depth study of the system performance revealed that, under available resources, the realistically achievable beam intensity is going to be comparable in both solutions. Taking into account simplicity and considerably lower costs of the passive beam forming system this solution was adopted. Optimization of the final system design was performed with a dedicated Geant4-based application created specifically for this purpose. The system is being currently fabricated at NCBJ.

In this paper the methodology, results as well as tools involved in the design of the specialized beam forming system will be presented.

Outline

Introduction and Motivation

- The LILLYPUT-3 accelerator at the Nondestructive Testing Laboratory (NTL) at Wroclaw Technology Park
- High-dose irradiation under cryogenic conditions (objectives, requirements, constraints, etc.)
- Electron beam forming active (scanning) VS passive (scattering)

Design of the system

- Beam scanning reality check
- Physics principles of dual foil system operation
- Simple analytical model of electron fluence
- Impact of helium filled applicator motivation for development of a MC model
- Geant4 model and tools for automatized design
- System optimization
- Calculation of expected dose rate

Conclusions and outlook

National Centre for Nuclear Research, Swierk, Poland

- \checkmark The largest research institute in Poland (1000+ employees)
- \checkmark Broad scope of fundamental and applied research
	- Nuclear physics (including reactor physics)
	- High energy physics (in collaboration with CERN and others)
	- Plasma physics
	- Material science
	- Free-electron lasers (in collaboration with XFEL)
- \checkmark Tradition of development and production of radiopharmaceuticals and medical equipment, including linear accelerators

NCBJ and electron LINACs for science, industry, medicine

Prototype cavities 1.3 GHz for Tesla-FEL at DESY

cavity for LINAC4@CERN

Prototype for mobile IOERT

Mobile linac for industrial radiography

Assembly of a medical linac

The LILLYPUT-3 accelerator at The Nondestructive Testing Laboratory at Wroclaw Technology Park

Standard radiographic configuration

- 6 and 9 MV X-ray beams
- Maximum dose rate 20 Gy/min
- Maximum field size *Φ*500mm @1m (adjustable with automatized jaw collimators)
- Digital imaging
- Automatized object table

Primary motivation

- Tests of radiation hardness of insulators (tens of MGy absorbed dose, cryogenic conditions)
- R&D in sterilization of polymer based medical products (tens of kGy)
- Research in polymer structure modifications (tens of kGy)

Perspectives, R&D opportunities

- Effects of irradiation on the structure of high temperature superconductors
- Effects of irradiation on the response time of electronic circuits
- Enhancement of optical properties of gemstones
- Coating hardening and regeneration
- Purification of exhaust gases from combustion of fossil fuels
- Food preservation

High-dose electron beam irradiation under cryogenic conditions at NTL

Primary motivation

• Tests of radiation hardness of insulators (tens of MGy absorbed dose, cryogenic conditions)

Objectives

- Irradiation of samples under cryogenic conditions (LN_2)
- Maximize dose rate (~ few tens of kGy/min). Total absorbed dose in the range of few tens of MGy.

Requirements

- Well flattened beam (i.e. homogenous dose distribution over sample area)
- Relatively small field size (~*Φ*80mm). Square samples ~60x60 mm

Approach towards system adaptation

- 9 MeV electron beam (extracted directly in a non-standard configuration)
- Shortest possible source to sample distance (SSD ~400 mm)
- Least possible disruption of the existing system

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Primary X-ray collimator

Radiation head in standard configuration

Movable X-ray jaw collimators (two pairs, X and Y axis)

Modular construction allows for reasonably simple removal of modules

Radiation head dismantled

Beam exit window Titanium, 0.05 mm

Target chamber

X-ray production targets can be moved in and out of beam path (in vacuum)

 $LN₂$ cryostat (holds irradiated samples)

Electron beam forming system – what is it good for?

Beam fluence at the exit window

- "pencil beam"
- very narrow (FWHM ~3 mm)
- extremely nonuniform

Desired beam fluence at sample location

- uniform over large area (*Φ* ~ 8 cm)

Common applications: sterilization, industrial material processing (e.g. polymer cross linking), modern hadron therapy

a High efficiency (→ high dose rate)
^{</sub> Relatively complex system (especiall}

- Relatively complex system (especially for 2D scanning)

S

Nontrivial to achieve uniform dose distribution
- Nontrivial to achieve uniform dose distribution
- \mathcal{F} Difficult to control beam uniformity

Common applications: sterilization, industrial material processing (e.g. polymer cross linking), modern hadron therapy

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- \mathbb{R} Relatively complex system (especially for 2D scanning)
 \mathbb{R} Nontrivial to achieve uniform dose distribution
- Nontrivial to achieve uniform dose distribution
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active = beam scanning passive = beam scattering and collimation

Common applications: electron beam therapy (also previous generation of proton therapy)

- Uniform beam distribution
- Simple, reliable
- **Significantly less efficient**

Common applications: sterilization, industrial material processing (e.g. polymer cross linking), modern hadron therapy

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Electron beam scanning – reality check

Electron beam scanning – reality check

Simple model of beam scanning on a $7x7$ cm² field with a beam of $FWHM = 45mm$

Common applications: sterilization, industrial material processing (e.g. polymer cross linking), hadron therapy

High efficiency (→ high dose rate)

- Relatively complex system (especially for 2D scanning)

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Common applications: electron beam therapy (also previous generation of proton therapy)

Beam exiting linacScattering foil ∧ SSD irradiation plane -20 -15 -10 -5 $\,$ 0 $\,$ $\overline{5}$ $10\,$ 15 -20 -15 -10 $\overline{5}$ $\overline{0}$ $\overline{}$ 10 15 20 20

The principle of dual-foil system

The principle of dual-foil system

Beam exiting linac

Calculation of electron fluence – simple model

Electron fluence at the position of the secondary foil due to scattering in the primary foil and in the air between foils

Component of the fluence at the irradiation plane due to a beamlet originating from rho at the second foil

Fluence at point \vec{r} at the irradiation plane Z_2 is a convolution of Φ_1 and Φ_2 :

$$
\Phi(Z_2, \vec{r}) = \int\limits_0^{2\pi} \int\limits_0^{\rho_{max}} \Phi_1(Z_1, \vec{\rho}) \Phi_2(Z_2, \vec{r}; Z_1, \vec{\rho}) \rho d\rho d\varphi
$$

Numerical integration is straight forward

Calculation of electron fluence – simple model

off-axis position at the irradiation plane (arb. units.)

Influence of the applicator on the electron distribution at the irradiation plane

Influence of the applicator on the electron distribution at the irradiation plane

The same scattering and flattening foils (MC calculation)

Without an applicator

With *Φ*93 mm circular applicator

Flatness calculated within *Φ*82 mm field Setup: exit window Ti 0.05 mm, 20 mm Air, scattering foil Ta 0.03 mm, 60 mm Air, flattening foil Al H=1mm, R=5.5 mm, SSD=400 mm

histogrammed at the end of the applicator. Flatness of the fluence distribution is calculated within the field as $flatness = \left(\frac{\Phi_{max}}{\Phi}\right)$ $\frac{\Phi_{max}}{\Phi_{min}} - 1$) · 100%

Dual-foil system: degrees of freedom

Parameters of the system:

- Beam energy fixed at 9 MeV
- Irradiation field size fixed at *Φ* 82 mm
- SSD fixed at 400 mm
- Scattering foil position $-$?
- Scattering foil material $-$?
- Scattering foil thickness ?
- Flattening foil material ?
- Flattening foil position ?
- Flattening foil thickness and width ?

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Dual-foil system: degrees of freedom

Parameters of the system:

- Beam energy fixed at 9 MeV
- Irradiation field size fixed at *Φ* 82 mm
- SSD fixed at 400 mm
- Scattering foil position as much upstream as possible – space for air cooling must be provided between the exit window and the scattering foil
- Scattering foil material $-$?
- Scattering foil thickness $-$?
- Flattening foil material $-$?
- Flattening foil position $-$?
- Flattening foil thickness and width $-$?

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Mass Scattering Power $\frac{T}{2}$ ρ $\sim \frac{Z^2}{4}$ \overline{A}

Collisional Stopping Power $S_{col} \sim \frac{Z}{4}$ \overline{A}

Scattering Foil

- The higher the Z the better (Bi, Pb, Au)
- High melting point (W, Ta)
- Availability, price (Ta)

Flattening Foil

- The higher the Z the better (Bi, Pb, Au)
- Feasible to machine a profiled shape (Al)

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- Scattering foil position as much upstream as possible – space for air cooling must be provided between the exit window and the scattering foil
- Scattering foil material Ta
- Scattering foil thickness $-$?
- Flattening foil material Al
- Flattening foil position $-$?
- Flattening foil thickness and width $-$?

• Minimal total energy degradation

Dual-foil system: degrees of freedom

Parameters of the system:

- Beam energy fixed at 9 MeV
- Irradiation field size fixed at *Φ* 82 mm
- SSD fixed at 400 mm
- Scattering foil position as much upstream as possible – space for air cooling must be provided between the exit window and the scattering foil
- Scattering foil material Ta
- Scattering foil thickness 0.03 mm (tentatively)
- Flattening foil material Al
- Flattening foil position **?**
- Flattening foil thickness and width **?**

A tool for automatized design optimization

Example of a flatness scan in function of aluminum flattening foil parameters H and R (at fixed scattering foil and separation distances)

An apology of a humble Jagiellonian University graduate

Let reason prevail over force

Assembly Hall of the Collegium Maius, Jagiellonian University, Kraków

Optimization of the Al flattening foil for the 0.03 mm Ta scattering foil

 H [mm]

Optimal Al flattening foil for the 0.03 mm Ta scattering foil

For comparison in the setup without the applicator Transmission 24.5% $< E > 8.48$ MeV

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Dual-foil system: scattering foil thickness

Thumb rule: total thickness of foils is minimal when the first foil thickness is such that, without the second foil, the fluence at the edge of the proposed irradiation field at SSD would be about 60% of the fluence on axis.

Ta 0.03 mm

• Minimal total energy degradation

Optimization of the Al flattening foil for the 0.01 mm Ta scattering foil.

 H [mm]

Minimal flatness R=6.5 mm H=1.85 mm

$$
h(r) = \mathit{Hexp}\left(-\frac{r^2}{R^2}\right)
$$

Depth Dose

"less degraded" VS "more degraded" energy spectrum

depth in water [mm]

Optimization of the Al flattening foil for the 0.01 mm Ta scattering foil.

 H [mm]

R=6 mm $H=1.5$ mm

$$
h(r) = \mathit{Hexp}\left(-\frac{r^2}{R^2}\right)
$$

Selected for production

Dose rate estimation (conservative)

 $\dot{D} = 284 \text{ Gy/s} = 17 \text{ kGy/min} = 1 \text{ MGy/h}$

Current state

- Passive forming could be equally efficient as scanning
- Dare to question known rules (of thumb)
- Dedicated Geant4 application with automation facility for rapid system development
- Optimum setup found via "brute force" multidimensional Monte Carlo optimization study
- Expected $\dot{\mathbf{D}} = 284 \text{ Gy/s} = 17 \text{ kgy/min} = 1 \text{ Mgy/h (at } \sim \phi 80 \text{mm field})$
- Most of the system components already fabricated at NCBJ
- Delivery, installation and tests at NTL@WPT expected in the second half of 2015

Thank you for your attention!