

Jagiellonian Symposium on Fundamental and Applied Subatomic Physics

# Development of a dedicated beam forming system for material and bioscience research with high intensity, small field electron beam of LILLYPUT 3 accelerator at Wroclaw Technology Park



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#### Abstract

The LILLYPUT 3 electron accelerator designed and manufactured at National Centre for Nuclear Research in Swierk, Poland (NCBJ) is the principal instrument of The Nondestructive Testing Laboratory at Wroclaw Technology Park.

The accelerator delivers 6 and 9 MeV electron beams. In a standard configuration the electron beam is converted into X-ray beam in a water cooled tungsten target. The primary use of the accelerator is nondestructive testing including R&D of novel techniques for industrial and medical imaging.

In addition, the high intensity electron beam can be directly extracted for a broad range of applications including material and bioscience research. For those applications a specialized beam forming system has been designed at NCBJ.

The purpose of this system is to deliver as high intensity electron beam as possible, while keeping beam flatness within 10% on a 7x7 sq. cm field in the distance of 40 cm from the beam exit window. Two alternative solutions were taken into consideration, one involving beam scanning and second based on passive beam forming with flattening foil. While it seemed that the highest beam intensity can be achieved by beam scanning, the in-depth study of the system performance revealed that, under available resources, the realistically achievable beam intensity is going to be comparable in both solutions. Taking into account simplicity and considerably lower costs of the passive beam forming system this solution was adopted. Optimization of the final system design was performed with a dedicated Geant4-based application created specifically for this purpose. The system is being currently fabricated at NCBJ.

In this paper the methodology, results as well as tools involved in the design of the specialized beam forming system will be presented.



### Outline

#### **Introduction and Motivation**

- The LILLYPUT-3 accelerator at the Nondestructive Testing Laboratory (NTL) at Wroclaw Technology Park
- High-dose irradiation under cryogenic conditions (objectives, requirements, constraints, etc.)
- Electron beam forming active (scanning) VS passive (scattering)

#### Design of the system

- Beam scanning reality check
- Physics principles of dual foil system operation
- Simple analytical model of electron fluence
- Impact of helium filled applicator motivation for development of a MC model
- Geant4 model and tools for automatized design
- System optimization
- Calculation of expected dose rate

#### **Conclusions and outlook**



# National Centre for Nuclear Research, Swierk, Poland



- ✓ The largest research institute in Poland (1000+ employees)
- ✓ Broad scope of fundamental and applied research
  - Nuclear physics (including reactor physics)
  - High energy physics (in collaboration with CERN and others)
  - Plasma physics
  - Material science
  - Free-electron lasers (in collaboration with XFEL)
- Tradition of development and production of radiopharmaceuticals and medical equipment, including linear accelerators



### NCBJ and electron LINACs for science, industry, medicine



Prototype cavities 1.3 GHz for Tesla-FEL at DESY



cavity for LINAC4@CERN



Prototype for mobile IOERT



Mobile linac for industrial radiography



Assembly of a medical linac



The LILLYPUT-3 accelerator at The Nondestructive Testing Laboratory at Wroclaw Technology Park





Standard radiographic configuration

- 6 and 9 MV X-ray beams
- Maximum dose rate 20 Gy/min
- Maximum field size Φ500mm @1m (adjustable with automatized jaw collimators)
- Digital imaging
- Automatized object table





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#### Primary motivation

- Tests of radiation hardness of insulators (tens of MGy absorbed dose, cryogenic conditions)
- R&D in sterilization of polymer based medical products (tens of kGy)
- Research in polymer structure modifications (tens of kGy)

#### Perspectives, R&D opportunities

- Effects of irradiation on the structure of high temperature superconductors
- Effects of irradiation on the response time of electronic circuits
- Enhancement of optical properties of gemstones
- Coating hardening and regeneration
- Purification of exhaust gases from combustion of fossil fuels
- Food preservation





# High-dose electron beam irradiation under cryogenic conditions at NTL

#### Primary motivation

• Tests of radiation hardness of insulators (tens of MGy absorbed dose, cryogenic conditions)

#### Objectives

- Irradiation of samples under cryogenic conditions (LN<sub>2</sub>)
- Maximize dose rate (~ few tens of kGy/min). Total absorbed dose in the range of few tens of MGy.

#### Requirements

- Well flattened beam (i.e. homogenous dose distribution over sample area)
- Relatively small field size (~ $\phi$ 80mm). Square samples ~60x60 mm

#### Approach towards system adaptation

- 9 MeV electron beam (extracted directly in a non-standard configuration)
- Shortest possible source to sample distance (SSD ~400 mm)
- Least possible disruption of the existing system



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#### Primary X-ray collimator

**Radiation head in standard configuration** 

Movable X-ray jaw collimators (two pairs, X and Y axis)



Modular construction allows for reasonably simple removal of modules

![](_page_10_Picture_0.jpeg)

![](_page_10_Picture_2.jpeg)

#### Radiation head dismantled

![](_page_10_Picture_4.jpeg)

Beam exit window Titanium, 0.05 mm

Target chamber

X-ray production targets can be moved in and out of beam path (in vacuum)

![](_page_11_Picture_0.jpeg)

![](_page_11_Picture_2.jpeg)

LN<sub>2</sub> cryostat (holds irradiated samples)

![](_page_12_Picture_0.jpeg)

## Electron beam forming system – what is it good for?

![](_page_12_Picture_2.jpeg)

#### Beam fluence at the exit window

- "pencil beam"
- very narrow (FWHM ~3 mm)
- extremely nonuniform

Desired beam fluence at sample location

- uniform over large area ( $\phi \sim 8 \text{ cm}$ )

![](_page_13_Picture_0.jpeg)

![](_page_13_Figure_2.jpeg)

Common applications: sterilization, industrial material processing (e.g. polymer cross linking), modern hadron therapy

### High efficiency ( $\rightarrow$ high dose rate)

- Relatively complex system (especially for 2D scanning)
- Nontrivial to achieve uniform dose distribution
- Difficult to control beam uniformity

![](_page_14_Picture_0.jpeg)

![](_page_14_Figure_2.jpeg)

Common applications: sterilization, industrial material processing (e.g. polymer cross linking), modern hadron therapy

#### High efficiency ( $\rightarrow$ high dose rate)

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- Difficult to control beam uniformity

#### passive = beam scattering and collimation

![](_page_14_Picture_9.jpeg)

Common applications: electron beam therapy (also previous generation of proton therapy)

- Uniform beam distribution
- Simple, reliable
- Significantly less efficient

![](_page_15_Picture_0.jpeg)

![](_page_15_Figure_2.jpeg)

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![](_page_15_Picture_9.jpeg)

Common applications: electron beam therapy (also previous generation of proton therapy)

- Uniform beam distribution
- Simple, reliable
- Significantly less efficient

![](_page_15_Picture_14.jpeg)

In this application, efficiency is all that matters

![](_page_15_Picture_16.jpeg)

![](_page_16_Picture_0.jpeg)

# **Electron beam scanning – reality check**

![](_page_16_Figure_2.jpeg)

![](_page_16_Figure_3.jpeg)

![](_page_17_Picture_0.jpeg)

# **Electron beam scanning – reality check**

Simple model of beam scanning on a 7x7 cm<sup>2</sup> field with a beam of FWHM = 45mm

![](_page_17_Figure_3.jpeg)

![](_page_18_Picture_0.jpeg)

![](_page_18_Figure_2.jpeg)

Common applications: sterilization, industrial material processing (e.g. polymer cross linking), hadron therapy

#### High efficiency ( $\rightarrow$ high dose rate)

- Relatively complex system (especially for 2D scanning)
- Nontrivial to achieve uniform dose distribution
- Difficult to control beam uniformity

![](_page_18_Picture_8.jpeg)

#### passive = beam scattering and collimation

![](_page_18_Picture_10.jpeg)

Common applications: electron beam therapy (also previous generation of proton therapy)

![](_page_18_Figure_12.jpeg)

![](_page_18_Picture_13.jpeg)

![](_page_19_Picture_0.jpeg)

![](_page_19_Figure_2.jpeg)

![](_page_20_Picture_0.jpeg)

![](_page_20_Figure_2.jpeg)

![](_page_21_Picture_0.jpeg)

# The principle of dual-foil system

![](_page_21_Figure_2.jpeg)

![](_page_22_Picture_0.jpeg)

## The principle of dual-foil system

Beam exiting linac

![](_page_22_Figure_3.jpeg)

![](_page_23_Picture_0.jpeg)

## Calculation of electron fluence – simple model

Electron fluence at the position of the secondary foil due to scattering in the primary foil and in the air between foils

Component of the fluence at the irradiation plane due to a beamlet originating from rho at the second foil

![](_page_23_Figure_4.jpeg)

![](_page_23_Figure_5.jpeg)

Fluence at point  $\vec{r}$  at the irradiation plane  $Z_2$  is a convolution of  $\Phi_1$  and  $\Phi_2$ :

$$\Phi(Z_2, \vec{r}) = \int_{0}^{2\pi} \int_{0}^{\rho_{max}} \Phi_1(Z_1, \vec{\rho}) \Phi_2(Z_2, \vec{r}; Z_1, \vec{\rho}) \rho d\rho d\varphi$$

Numerical integration is straight forward

![](_page_24_Picture_0.jpeg)

![](_page_24_Figure_2.jpeg)

![](_page_25_Picture_0.jpeg)

# Influence of the applicator on the electron distribution at the irradiation plane

![](_page_25_Picture_2.jpeg)

![](_page_25_Picture_3.jpeg)

![](_page_26_Picture_0.jpeg)

# Influence of the applicator on the electron distribution at the irradiation plane

The same scattering and flattening foils (MC calculation)

Without an applicator

With  $\phi$ 93 mm circular applicator

![](_page_26_Figure_5.jpeg)

Flatness calculated within  $\Phi$ 82 mm field Setup: exit window Ti 0.05 mm, 20 mm Air, scattering foil Ta 0.03 mm, 60 mm Air, flattening foil AI H=1mm, R=5.5 mm, SSD=400 mm

![](_page_27_Figure_0.jpeg)

```
chamber
holder
```

Electron fluence and energy are histogrammed at the end of the applicator. Flatness of the fluence distribution is calculated within the field as  $flatness = \left(\frac{\Phi_{max}}{\Phi_{min}} - 1\right) \cdot 100\%$ 

![](_page_28_Picture_0.jpeg)

## Dual-foil system: degrees of freedom

![](_page_28_Figure_2.jpeg)

Parameters of the system:

- Beam energy fixed at 9 MeV
- Irradiation field size fixed at  $\phi$  82 mm
- SSD fixed at 400 mm
- Scattering foil position -?
- Scattering foil material -?
- Scattering foil thickness -?
- Flattening foil material -?
- Flattening foil position ?
- Flattening foil thickness and width ?

![](_page_29_Picture_0.jpeg)

## Dual-foil system: degrees of freedom

![](_page_29_Figure_2.jpeg)

Parameters of the system:

- Beam energy fixed at 9 MeV
- Irradiation field size fixed at  $\phi$  82 mm
- SSD fixed at 400 mm
- Scattering foil position as much upstream as possible – space for air cooling must be provided between the exit window and the scattering foil
- Scattering foil material -?
- Scattering foil thickness ?
- Flattening foil material -?
- Flattening foil position -?
- Flattening foil thickness and width -?

![](_page_30_Picture_0.jpeg)

Mass Scattering Power  $\frac{T}{\rho} \sim \frac{Z^2}{A}$ 

Collisional Stopping Power  $S_{col} \sim \frac{Z}{A}$ 

Scattering Foil

- The higher the Z the better (Bi, Pb, Au)
- High melting point (W, Ta)
- Availability, price (Ta)

Flattening Foil

- The higher the Z the better (Bi, Pb, Au)
- Feasible to machine a profiled shape (AI)

![](_page_31_Picture_0.jpeg)

## Dual-foil system: degrees of freedom

![](_page_31_Figure_2.jpeg)

Parameters of the system:

- Beam energy fixed at 9 MeV
- Irradiation field size fixed at  $\phi$  82 mm
- SSD fixed at 400 mm
- Scattering foil position as much upstream as possible – space for air cooling must be provided between the exit window and the scattering foil
- Scattering foil material Ta
- Scattering foil thickness ?
- Flattening foil material Al
- Flattening foil position -?
- Flattening foil thickness and width -?

![](_page_32_Figure_0.jpeg)

# **Dual-foil system: scattering foil thickness**

Thumb rule: total thickness of foils is minimal when the first foil thickness is such that, without the second foil, the fluence at the edge of the proposed irradiation field at SSD would be about 60% of the fluence on axis.

![](_page_32_Figure_3.jpeg)

Ta 0.03 mm

![](_page_32_Figure_5.jpeg)

Minimal total energy degradation

![](_page_33_Picture_0.jpeg)

## Dual-foil system: degrees of freedom

![](_page_33_Figure_2.jpeg)

Parameters of the system:

- Beam energy fixed at 9 MeV
- Irradiation field size fixed at  $\phi$  82 mm
- SSD fixed at 400 mm
- Scattering foil position as much upstream as possible – space for air cooling must be provided between the exit window and the scattering foil
- Scattering foil material Ta
- Scattering foil thickness 0.03 mm (tentatively)
- Flattening foil material Al
- Flattening foil position -?
- Flattening foil thickness and width ?

![](_page_34_Picture_0.jpeg)

### A tool for automatized design optimization

![](_page_34_Figure_2.jpeg)

![](_page_35_Picture_0.jpeg)

Example of a flatness scan in function of aluminum flattening foil parameters H and R (at fixed scattering foil and separation distances)

![](_page_35_Figure_3.jpeg)

![](_page_36_Figure_0.jpeg)

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### An apology of a humble Jagiellonian University graduate

![](_page_37_Picture_1.jpeg)

### Let reason prevail over force

Assembly Hall of the Collegium Maius, Jagiellonian University, Kraków

### Optimization of the AI flattening foil for the 0.03 mm Ta scattering foil

H [mm]

![](_page_38_Figure_3.jpeg)

![](_page_38_Figure_4.jpeg)

![](_page_39_Picture_0.jpeg)

### Optimal AI flattening foil for the 0.03 mm Ta scattering foil

![](_page_39_Figure_2.jpeg)

For comparison in the setup without the applicator Transmission 24.5%  $\langle E \rangle = 8.48 \text{ MeV}$ 

9

![](_page_40_Figure_0.jpeg)

# **Dual-foil system: scattering foil thickness**

Thumb rule: total thickness of foils is minimal when the first foil thickness is such that, without the second foil, the fluence at the edge of the proposed irradiation field at SSD would be about 60% of the fluence on axis.

![](_page_40_Figure_3.jpeg)

Ta 0.03 mm

![](_page_40_Figure_5.jpeg)

Minimal total energy degradation

![](_page_41_Picture_0.jpeg)

#### Optimization of the AI flattening foil for the 0.01 mm Ta scattering foil.

H [mm]

![](_page_41_Figure_3.jpeg)

R [mm]

![](_page_42_Picture_0.jpeg)

Minimal flatness R=6.5 mm H=1.85 mm

$$h(r) = Hexp\left(-\frac{r^2}{R^2}\right)$$

![](_page_42_Figure_4.jpeg)

![](_page_43_Picture_0.jpeg)

### **Depth Dose**

"less degraded" VS "more degraded" energy spectrum

![](_page_43_Figure_3.jpeg)

depth in water [mm]

![](_page_44_Picture_0.jpeg)

#### Optimization of the AI flattening foil for the 0.01 mm Ta scattering foil.

H [mm]

![](_page_44_Figure_3.jpeg)

![](_page_45_Picture_0.jpeg)

R=6 mm H=1.5 mm

$$h(r) = Hexp\left(-\frac{r^2}{R^2}\right)$$

![](_page_45_Figure_4.jpeg)

Selected for production

![](_page_46_Picture_0.jpeg)

## **Dose rate estimation (conservative)**

![](_page_46_Figure_2.jpeg)

 $\dot{D} = 284 \text{ Gy/s} = 17 \text{ kGy/min} = 1 \text{ MGy/h}$ 

![](_page_47_Picture_0.jpeg)

### **Current state**

![](_page_47_Picture_2.jpeg)

![](_page_48_Picture_0.jpeg)

- Passive forming could be equally efficient as scanning
- Dare to question known rules (of thumb)
- Dedicated Geant4 application with automation facility for rapid system development
- Optimum setup found via "brute force" multidimensional Monte Carlo optimization study
- Expected  $\dot{D} = 284 \text{ Gy/s} = 17 \text{ kGy/min} = 1 \text{ MGy/h}$  (at ~ $\phi$ 80mm field)
- Most of the system components already fabricated at NCBJ
- Delivery, installation and tests at NTL@WPT expected in the second half of 2015

![](_page_49_Picture_0.jpeg)

# Thank you for your attention!